

FACTORY OF ELECTRIC APPARATUS

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ELECTROMAGNETIC DISC BRAKES H2SPX series with constant braking torque





K-EN-H2SPX-20151203

Spring actuated and electromagnetically released disk brake type H2SPX powered by direct current. Designed for braking rotating machine parts and their precision positioning. Utilized as safety brake. High repeatability even with large number of actuations. The brake characterizes relatively simple construction, facility for regulating brake parameters such as braking torque, braking time and also possibility of supply from alternating current source after connecting up a rectifier circuit delivered at customer's request along with the brake. An additional feature is quiet operation, particularly important when the equipment is operated by a number of drives operating additionally with high frequency of actuations. Brake design guarantees simple and problem-free installation. Various options of executions are at disposal with respect to fittings/accessories, brake supply, climatic conditions of utilization, enabling selection of appropriate option for definite utilization conditions



They are designed for braking rotating parts of machines and their task is:

- emergency stopping, in order to ensure drive safety functions,
- immobilizing machine actuators, acting as a positioning device,
- minimizing run-on times of drives (to meed safety requirements according to Office of Technical Inspection (UDT) regulations,
- built onto an electric motor, the brake provides a self-braking motor, a drive unit meeting the requirements of utilisation safety and positioning.

Brakes can be manufactured in variants suitable for various direct-current voltages: 24V, 104V, 180V, 207V which allows them to be supplied from standard alternating current sources, through appropriate rectifier.

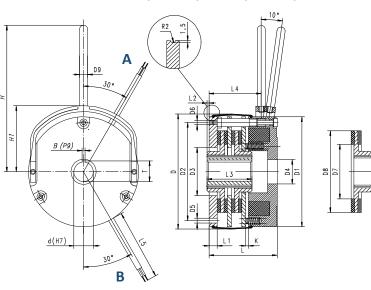
Parameters			Unit		Brake type										
				H2SPX 63	H2SPX 71	H2SPX 80	H2SPX 90	H2SPX 100	H2SPX 112	H2SPX 132	H2SPX 160	H2SPX 180	H2SPX 200	H2SPX 280	H2SPX 315
Sup	ply voltage	Un	[V]					24, 104,	180, 207					24, 10	4,180
Pow	ver	$P_{20^{\circ}}$	[W]	20	25	30	30	40	50	55	65	75	100	250	340
Bral	king torque	M_{h}	[Nm]	7	13	26	26	50	100	160	240	400	700	1600	2500
Max	x. speed	n _{max}	min ⁻¹		3000										
Wei	ght	G	[kg]	0,7	1,9	3,5	3,5	6,8	7,8	11,8	18,0	25,3	30,0	85,0	126,0
	bient perature	Т	⁰ C		-25 ÷ +40										
*	On direct voltage	t 0,1	ms	35	65	90	90	120	150	180	300	400	500	500	600
time	side	t0,9	1115	17	35	40	40	50	65	90	110	200	270	300	500
ating	On	t0,1		35	65	90	90	120	150	180	300	400	500	500	600
On alternating voltage sideto,1 to,935659090120150Brake disconnection on alternating current side cau respect to disconnection							-	n in braki	ng time t	09 with					

 $t_{0,1}$ - releasing time (from switching on current to drop in braking torque to 10% M_{nom})

t_{0,9} - braking time (from switching off current to attaining 90% M_{nom})

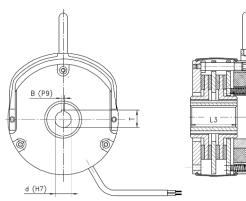
*) Values of releasing and braking times are given as approximations, since they depend on mode of assembly/installation, temperature and power supply.

Cable output: A - H2SPX100, H2SPX112, H2SPX132, H2SPX160, H2SPX180, H2SPX280, H2SPX315 B - H2SPX63, H2SPX71, H2SPX80, H2SPX90, H2SPX200



Туре	M _h [Nm]	D	D1	D2	D3	D4	D5	D6	D7	D8	D9	L	L1	L2	L3	L4	L5	L6	L7	K	Н	H1
H2SPX63	7	91	84	72	25	23,4	Ø4,5x3	M4x3	47	62	8	41	6	0	25	37	450	6,7	1,0	0,2	100	51
H2SPX71	13	110	102	90	30	30,4	Ø5,5x3	M5x3	59	76	8	48	7	4	48	40	450	6,7	1,0	0,2	115	61
H2SPX80	26	133	125	112	44	40,4	Ø6,4x3	M6x3	61	95	10	58	9	3	55	53	450	9,0	1,0	0,2	170	73
H2SPX90	26	133	125	112	44	40,4	Ø6,4x3	M6X3	61	95	10	58	9	3	55	53	450	9,0	1,0	0,2	170	73
H2SPX100	50	156	148	132	45	48,4	Ø6,4x3	M6x3	74	114	10	66	9	5	65	59	450	9,0	1,0	0,3	184	94
H2SPX112	100	170	162	145	55	58,3	Ø8,4x3	M8x3	90	124	12	76	11	8	75	63	450	9,0	2,0	0,3	191	102
H2SPX132	160	196	188	170	84	66,4	Ø8,4x3	M8x3	100	154	12	83	11	8	75	63	450	9,0	2,0	0,3	204	116
H2SPX160	240	223	215	196	104	82,8	Ø9,0x4	M8x6	130	176	12	91	11	16	92	82	450	11,0	2,0	0,3	230	129
H2SPX180	400	262	252	230	134	87,8	Ø11x6	M10x6	148	207	14	110	11	16	105	94	800	11,0	2,0	0,5	339	157
H2SPX200	700	314	302	278	120	132,8	Ø11x6	M10x6	198	255	14	122	12,5	19	115	113	800	11,0	2,0	0,5	466	182
H2SPX280	1600	356	342	308	150	150,0	Ø13x6	M12x6	200	270	20	157	25	42	160	135	1500	11,0	3,0	0,6	408	206
H2SPX315	2500	412	400	360	170	170,0	Ø13x6	M12x6	210	300	20	171	25	52	180	143	1500	13,5	3,0	0,6	434	232

Geared bushing hole diameters



Туре	d	В	Т	d _{max}	d _{smax} *	L3
H2SPX63	15	5	17,3	15		25
H2SPX71	15	5	17,3	15		48
H2SPX80	19	6	21,8	25		55
H2SPX90	19	6	21,8	25		55
H2SPX100	25	8	28,3	25		65
H2SPX112	25	8	28,3	35**		75
H2SPX132	35**	8	38,3	35**		75
H2SPX160	40	12	43,3	45	50	92
H2SPX180	42	12	45,3	45	50	105
H2SPX200	42	12	45,3	45	75	115
H2SPX280	55	16	59,3	75		160
H2SPX315	70	20	74,9	100		180

d - standard geared bushing hole diameters

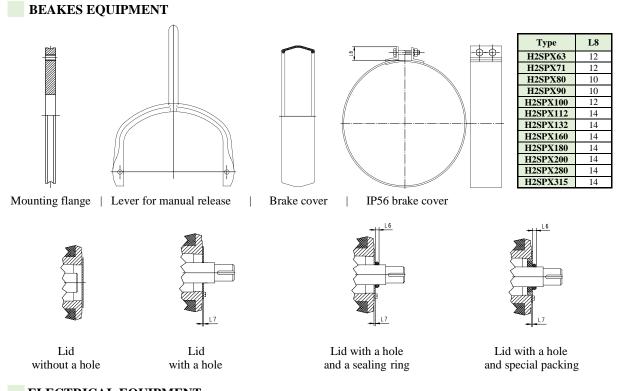
d smax - maximum geared bushing hole diameters

d* smax - at extra charge it is possible to manufacture the brakes with the specially increased diameter of the gear hub -for the H2SPX112 and H2SPX132 brakes and for the geared bushing hole diameters from 32 to 35mm, the key groove with the width of 8 mm (the width of the groove is incompatible with PN/M-85005 and DIN 6885 standards)

Normalized hole diameter ranges



Hole diameter [mm]	В	t 2
above - to		
10 - 12	4	1,8
12 – 17	5	2,3
17 – 22	6	2,8
22 - 30	8	3,3
30 - 38	10	3,3
38 - 44	12	3,3
44 - 50	14	3,8
50 - 58	16	4,3
58 - 65	18	4,4
65 - 75	20	4,9
75 - 85	22	5,4
85 - 95	25	5,4
95 -110	28	6,4



ELECTRICAL EQUIPMENT

A number of modules, ranging from simple circuits with classic designs, to complex assemblies ensuring quick action and drives positioning have been designed to drive the brakes. Relevant brake applications with switching in the primary or secondary circuits are ensured by half- or full-wave rectifiers and fast electronic circuits. The manufacturer recommends to use as low alternating current voltages as possible to supply the brakes. Appropriate choice of the control voltage will prevent or at least limit surges that may occur in power supply circuits. It is not recommended to use extensively long control wiring, which would be a source of harmful surges.

Rectifier B2-1P

The B2–1P rectifiers series forms a complete wave rectifier unit for direct installation. The terminal strip provided facilitates installation and connection to the circuit.

Rectifier B2-1P cooperates with brakes H2SPX63 ÷ H2SPX200.

RECTIFIEF	R PARAM	For example					
		B2-1P-400 B2-1P-600 Maximum in		Maximum input voltage			
Maximum input voltage (alternating voltage AC)	$U_{\rm IN}$	400 VAC	600 VAC	(alternating voltage) - $U_{\rm IN} = 230 {\rm VAC}$,			
Maximum output voltage (direct voltage DC)	Uout	0,45 U _{IN}	$0,45U_{\rm IN}$	The resulting output voltage of the rectifier (direct voltage) - $0.45U_{IN}=0.45 \times 230=104VDC$			
Maximum continuous output current rectifier	IOUT	2A	2A	(unect voltage) - 0,450IN-0,45 x 250-104 VDC			

Rectifier B5-1P

The B5–1P rectifiers series forms a complete wave rectifier unit for direct installation. The terminal strip provided facilitates installation and connection to the circuit.

Rectifier B5-1P cooperates with brakes H2SPX63 ÷ H2SPX315.

RECTIFIER PARAMETERS							
		B5-1P-400	B5-1P-600				
Maximum input voltage (alternating voltage AC)	UIN	400 VAC	600 VAC				
Maximum output voltage (direct voltage DC)	Uout	0,45 U _{IN}	$0,45U_{\rm IN}$				
Maximum continuous output current rectifier	IOUT	5A	5A				

For example

Maximum input voltage (alternating voltage) - $U_{IN} = 230VAC$,

The resulting output voltage of the rectifier (direct voltage) - $0.45 U_{IN} = 0.45 \text{ x } 230 = 104 \text{VDC}$

Rectifier B2-2P

The B2–2P rectifiers series forms a complete full-wave rectifier unit for direct installation. The terminal strip provided facilitates installation and connection to the circuit. The rectifier allows feeding input voltage max. 400VAC, 2A which after rectification provides DC voltage of value equal to 0,9 input voltage.

Rectifier B2-2P cooperates with brakes H2SPX63 ÷ H2SPX200.

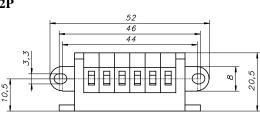
RECTIFIER PARAMETERS							
Maximum input voltage (alternating voltage AC)	$U_{\rm IN}$	250 VAC					
Maximum output voltage (direct voltage DC)	Uout	$0,9U_{\rm IN}$					
Maximum continuous output current rectifier	Iout	2A					

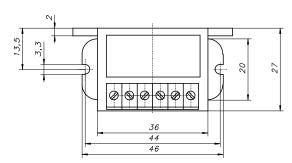
For example

Maximum input voltage (alternating voltage) - $U_{IN} = 230$ VAC, The resulting output voltage of the rectifier (direct voltage) - $0.9U_{IN} = 0.9$ x 230=207VDC

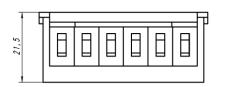
Rectifiers dimensions

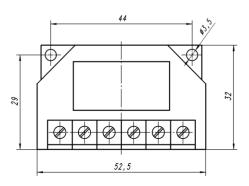
B2-1P-400, B5-1P-400, B2-2P





B2-1P-600, B5-1P-600



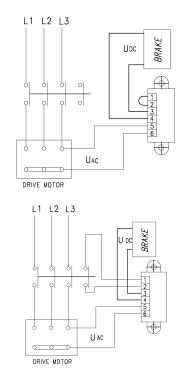


Disconnection of power supply on AC side

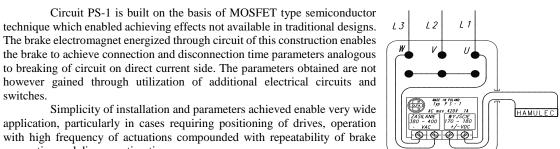
The diagram presents connection of rectifiers to supply circuit of motor. When disconnecting the voltage, the magnetic field causes the coil current to flow further through the rectifying diodes and drops slowly. The magnetic field reduces gradually causing prolonged time of braking action and consequently delayed increase of braking torque. If action time is irrelevant, brake should be connected on the AC side. When switching off, the supply circuits act as rectifying diodes.

Disconnection of power supply on DC side

The diagram presents connection of rectifiers into electric motor circuit. The coil current is interrupted between the coil and supply (rectifier) circuit. The magnetic field reduces very quickly, **giving short time of braking action and consequently rapid growth of braking torque**. When switching off on DC voltage side, a high peak voltage is generated in the coil causing faster wear of contacts due to sparking. For protecting the coil against peak voltages and protecting the contacts against excessive wear, the rectifier circuit is provided with protective facility allowing brake connection on DC voltage side.



Rectifier PS-1



however gained through utilization of additional electrical circuits and switches. Simplicity of installation and parameters achieved enable very wide application, particularly in cases requiring positioning of drives, operation with high frequency of actuations compounded with repeatability of brake

The brake electromagnet energized through circuit of this construction enables the brake to achieve connection and disconnection time parameters analogous to breaking of circuit on direct current side. The parameters obtained are not

Circuit PS-1 is built on the basis of MOSFET type semiconductor

Supply circuit PS-1 forms a complete unit for direct installation. Provided with a four-terminal strip, it enables unhindered adaptation in every cooperating circuit. The circuit is adapted for supply from alternating current source of 380-400 VAC max. 420 VAC which after rectification and appropriate formation enables obtaining direct voltage of 170-180 VDC for brake supply.

The diagram below shows the method of connecting the circuit PS 1 into supply circuit of brake cooperating with 3x400 VAC electric motor with star-connected winding.

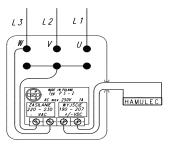
Rectifier PS-1 cooperates with brakes H2SPX63 ÷ H2SPX180.

Rectifier PS-2

connecting and disconnecting times.

Circuit PS-2 is built on the basis of MOSFET type semiconductor technique which enabled achieving effects not available in traditional designs. The brake electromagnet energized through circuit of this construction enables the brake to achieve connection and disconnection time parameters analogous to breaking of circuit on direct current side. The parameters obtained are not however gained through utilization of additional electrical circuits and switches.

Simplicity of installation and parameters achieved enable very wide application, particularly in cases requiring positioning of drives, operation with high frequency of actuations compounded with repeatability of brake connecting and disconnecting times.

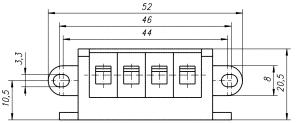


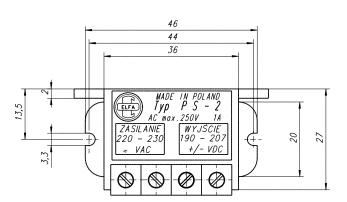
Supply circuit PS 2 forms a complete unit for direct installation. Provided with a four-terminal strip, it enables unhindered adaptation in every cooperating circuit. The circuit is adapted for supply from alternating current source of 220-230 VAC max. 250 VAC which after rectification and appropriate formation enables obtaining direct voltage of 190-207 VDC for brake supply.

The diagram below shows the method of connecting the circuit PS 2 into supply circuit of brake cooperating with 3x400 VAC electric motor with star-connected winding.

cooperates with brakes H2SPX63 ÷ H2SPX200.

Rectifiers PS-1, PS-2 dimensions



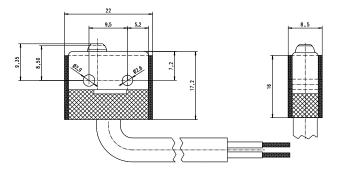


CONTROL AND SIGNALING CIRCUTS – microswitches

Having in mind the user who requires the control of the brake, we have designed special signaling and control circuits, which enable to control the state of the brake (engaged, disengaged) and the wear of the plate lining. The usage of these circuits enables to control the brake with the use of automatic elements, which ensure high level of safety and reliability. Due to its compact design, the microswitch can be used in any other applications, as long as its parameters meet design requirements.

MICROSWITCHES - ELECTRIC PARAMETERS								
Switch parameter	Switch KZ	Switch KO						
Max. voltage AC	250 V AC	250 V AC						
Max. AC switching current	5 A	6 A						
Max. Voltage DC	28V DC	220V DC						
Max. DC switching current	3 A / 28V DC	6A / 12V DC 3A / 24V DC 1A / 60V DC 0,5A / 110V DC 0,25A / 220V DC						
Protection rating	IP 66	IP 66						
Terminals	NO /NC	NO /NC						

MICROSWITCH DIMENSIONS



KO

K7

SAMPLE INSTALATION

Response monitoring microswitch $- \mathbf{KZ}$ - control of the state of brake (engaged, disengaged),

Microswitch of the brake lining control – \mathbf{KO} – the microswitch indicates approaching the maximum wear of the brake disc and the necessity of the brake's regulation or replacement of the disc brake, which enables further work of the brake. The regulation procedure is described in the brake operating manual.

Response monitoring microswitch and microswitch of the brake lining control – KZ+KO

Microswitches set **KZ+KO** is available from type H2SPX80 inclusive.

PROCTECTIVE CIRCUITS – thermal protection

To protect electromagnet windings against heat build-up (slow-changing overloads) thermal sensor are used. In our offer we have PTC thermistors, which feature high resistance gradients when their rated temperature is reached - posistors - P or bimetallic thermal sensor - B.

Posistor-based sensors are made in the form of an insulated pill with connecting wires extending inside a teflon insulation, installed directly on the electromagnet windings. Sensor circuit terminals are routed outside the brake to the terminal box and connected to a separate connection block or terminal strip. So-called resistance relays are intended for thermistor-based PTC temperature sensors. When temperature of at least one of the sensors rises above the rated value, the circuit resistance suddenly increases triggering the relay.

Posistor thermal protection – P

Note! PTC sensor terminals must not be connected directly to the contactor.

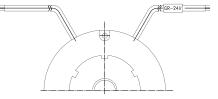
The brake protection has the form of a bimetallic sensor. Brake operation is controlled by a sensor or by a set of sensors, which ensure its safe operation; excessive temperature indication is obtained from the thermal switch installed inside the brake electromagnet's housing rated for a specific temperature. When the limit temperature for the sensor is exceeded, the information for the automatic control equipment is sent or the brake circuit is disconnected.

Bimetallic thermal protection – B

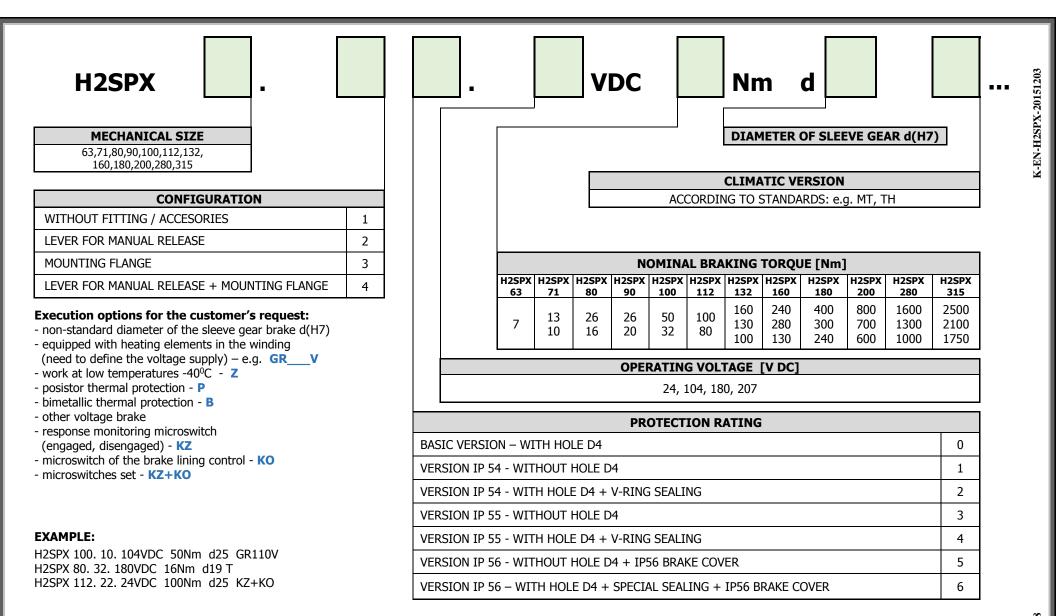
AUXILIARY CIRCUITS – anti-condensation heaters

The so-called parking heating is used to prevent vapours condensation inside the brake. The equipment is particularly useful in negative temperatures or in high humidity environments. The heater is supplied through its dedicated pair of wires. The heater power supply voltage matches customer requirements. – <u>the need to define the voltage during order</u>.

Anti-condensation heaters – **GR** – ____V



SAMPLE INSTALATION



The producer reserves the right to modify as a result of developing the product. It is possible to realize special versions. Page 8 from 8